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*Technical Memorandum 33-770*

*C'—Compatible Interpolation  
Over a Triangle*

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JET PROPULSION LABORATORY  
CALIFORNIA INSTITUTE OF TECHNOLOGY  
PASADENA, CALIFORNIA

May 1, 1976



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## Preface

The work described herein was performed by the Data Systems Division of the Jet Propulsion Laboratory.

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### **Abstract**

An elementary derivation and a complete description are given of an algorithm for interpolation over a plane triangle when function values and first partial derivatives are given at the vertices. The method gives  $C^1$  continuity with neighboring triangles.

The interpolation method is mathematically equivalent to one that has been discussed previously in the literature; however, the algorithmic form given here is more efficient than has previously been described.

# $C^1$ - Compatible Interpolation Over A Triangle

## 1. Introduction

The problem treated in this report has been treated by numerous authors. See Birkhoff and Mansfield [1974] for extensive discussion of this and closely related problems and for other references.  $C^1$  interpolation over triangular grids has application in structural analysis via finite element methods and in the computerized representation of surfaces for computer aided design.

The problem also arises in diverse scientific and engineering fields where it is useful to be able to construct a smooth surface that passes through a finite set of observed or computed values of some function  $z = f(x, y)$ . In these data-fitting applications, the desired end-product is often a contour plot of the interpolated function.

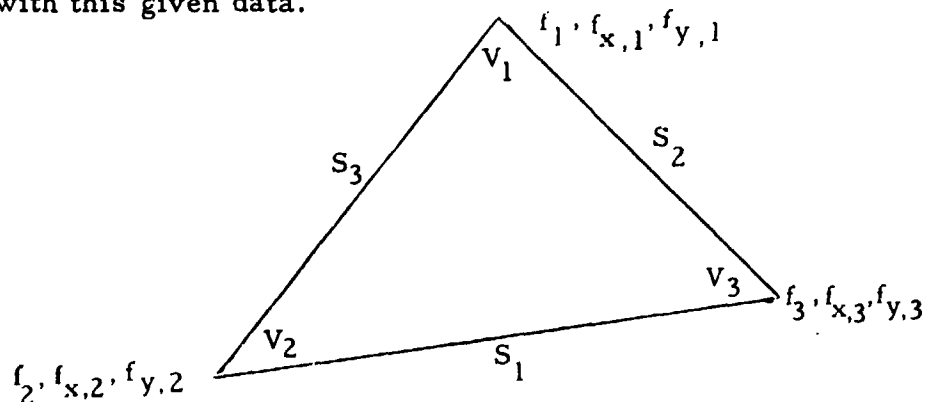
In this report, we give an elementary derivation and a complete algorithmic description of an interpolation method that is mathematically equivalent to one that is mentioned by Birkhoff and Mansfield, [1974], and specified in detail by J.-J. Goël, [1968]. Goël attributes the method to Clough and Tocher [1965] and Zienkiewicz [1967].

The algorithmic form in which the method is given here is more efficient for solving the interpolation problem than the form given by Goël [1968]. It is my present conjecture that one cannot expect to discover an algorithm for this problem that is significantly more efficient than the one given here. Other reports, yet to be written, will deal with the integration of this interpolation algorithm into a set of subprograms for constructing a triangular grid, Lawson [1972], and then doing look-up,  $C^1$  interpolation, and contour plotting for a function,  $z = f(x, y)$ , whose values are given at a finite set of points.

The author thanks Dr. Fred T. Krogh for numerous fruitful discussions during the exploratory phase that preceded the writing of this paper and for a critical reading of the paper that produced numerous improvements.

2. The problem of  $C^1$  - compatible interpolation over a triangle

Assume that values of a function,  $f$ , and its first partial derivatives,  $f_x$  and  $f_y$ , are given at the three vertices of a triangle,  $T$ , in the  $(xy)$ -plane. We wish to define a function  $w(x, y)$  for  $(x, y)$  in the triangle,  $T$ , that will agree with this given data.



With nine items of data being given we may anticipate that the interpolation method can be required to be exact for all polynomial functions of degree up to two, but not for all cubic functions, since the set of quadratic functions in two variables is a six-parameter family while the set of all cubics is a ten-parameter family. We will impose the requirement that the method be exact for quadratic polynomial data.

Furthermore we want the interpolation method to have the property that if it is applied to two adjacent triangles having an edge in common then function values and the first partial derivatives of the two interpolated functions will be identical along the common edge. Thus the method can be used for interpolation over a triangular grid, and the surface defined by the totality of the locally interpolated functions will have  $C^1$  continuity over the entire region covered by the grid.

A convenient way of assuring that the interpolated functions on adjacent triangles have the same values and first partial derivatives along the common edge is to require that the values and first partial derivatives of the interpolated function along any edge must be determined only by the data given on that edge, i. e. the data given at the vertices at the ends of that edge.

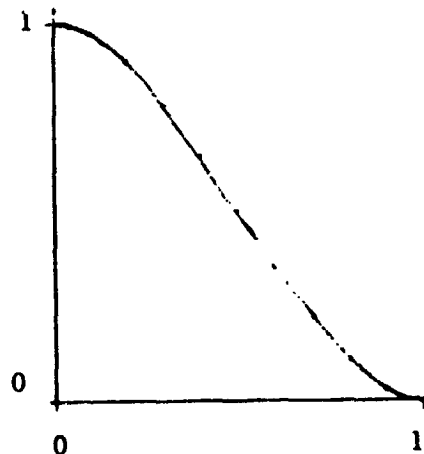
Relative to a particular edge, say  $S_1$ , the given partial derivatives at vertices  $V_2$  and  $V_3$  can be rotated to give partial derivatives tangential to the edge and normal to the edge at  $V_2$  and  $V_3$ . A fairly natural approach is to define values of  $w$  along side  $S_1$  by Hermite cubic interpolation matching the required function values and tangential first partial derivative values at  $V_2$  and  $V_3$ , and to define the first partial derivative of  $w$  normal to side  $S_1$  to be a linear function along side  $S_1$ , taking the required values at  $V_2$  and  $V_3$ .



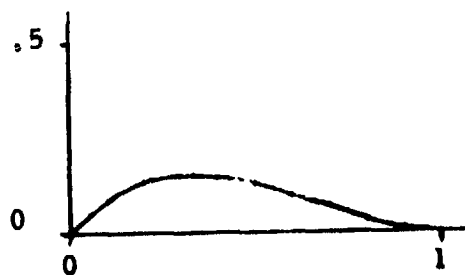
3. Some observations on one-dimensional Hermite cubic interpolation

Consider Hermite cubic interpolation on the unite interval  $0 \leq x \leq 1$ , with given data  $f_0$  and  $f'_0$  at  $x = 0$  and  $f_1$  and  $f'_1$  at  $x = 1$ . The cardinal functions for this data are

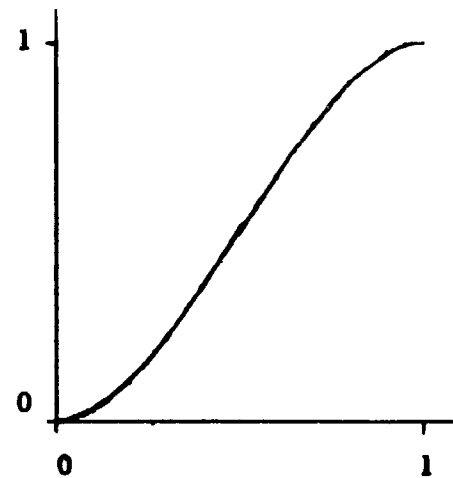
(1)  $\varphi_0(x) = (2x+1)(x-1)^2$



(2)  $\bar{\varphi}_0(x) = x(x-1)^2$

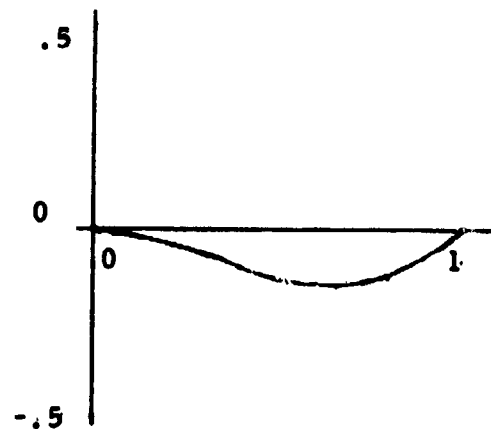


$$(3) \quad \varphi_1(x) = \varphi_0(1-x)$$



and

$$(4) \quad \bar{\varphi}_1(x) = -\bar{\varphi}_0(1-x)$$



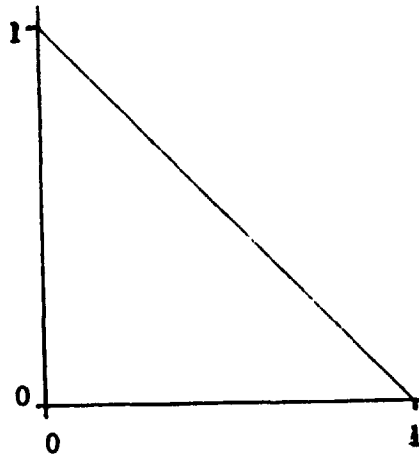
The interpolated cubic polynomial is given by

$$(5) \quad w(x) = f_0 \varphi_0(x) + f'_0 \bar{\varphi}_0(x) + f_1 \varphi_1(x) + f'_1 \bar{\varphi}_1(x)$$

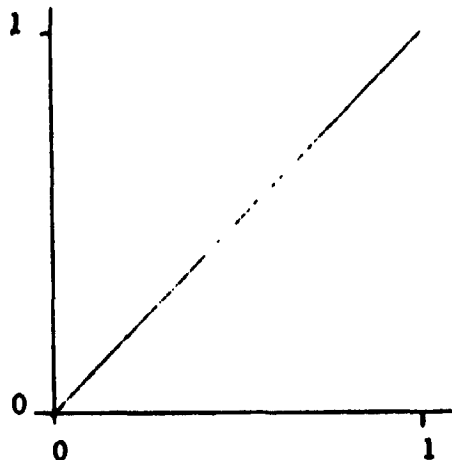
Note that all four of the cardinal functions in this formulation are cubic polynomials. In our interpolation problem over a triangle we shall find that cardinal functions of degree higher than two introduce relatively large increases in computational complexity. Thus it is useful to note that the solution to the one-dimensional Hermite cubic interpolation problem can be rearranged (in various ways) to involve at most one cubic basis function.

For example, we can use the four functions:

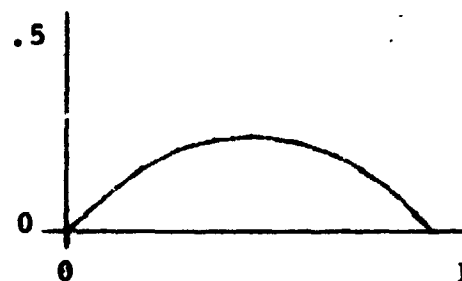
$$(6) \quad \psi_1(x) = 1-x$$



$$(7) \quad \hat{\psi}_1(x) = x$$



$$(8) \quad \psi_2(x) = x(1-x)$$



and

$$(9) \quad \psi_3(x) = 2x(x - \frac{1}{2})(x-1)$$



The same cubic polynomial as is defined by Eq (5) can then be constructed using the formulas

$$(10) \quad m = f_1 - f_0$$

$$(11) \quad w(x) = f_0 \psi_1(x) + f_1 \hat{\psi}_1(x) + \frac{f'_0 - f'_1}{2} \psi_2(x) + \frac{f'_1 + f'_0 - 2m}{2} \psi_3(x)$$

Eq (11) is easily derived by constructing the formula in two stages. The first two terms clearly provide the linear interpolant that matches the data  $f_0$  and  $f_1$  at 0 and 1 respectively. This linear function has a slope of  $m = f_1 - f_0$ .

Thus, after subtracting this linear function, the remaining problem is to determine a cubic function having zero values at the endpoints and slopes of  $f'_0 - m$  at 0 and  $f'_1 - m$  at 1. Since  $\psi_2$  has slopes of 1 and -1 at 0 and 1 respectively and  $\psi_3$  has a slope of 1 at both 0 and 1 it follows that the function

$$(12) \quad \frac{(f'_0 - m) - (f'_1 - m)}{2} \psi_2(x) + \frac{(f'_0 - m) + f'_1 - m}{2} \psi_3(x)$$

will fit the residual data.

Combining this two-stage procedure into a single formula gives Eq (11).

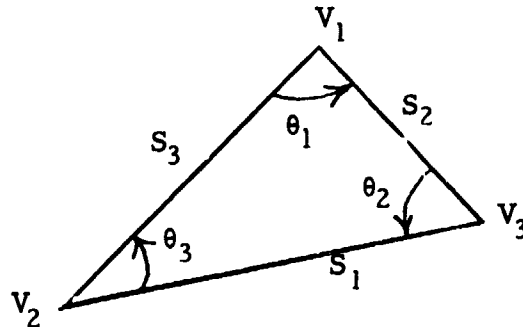
An analagous approach of combining a linear interpolant with a quadratic part and then a cubic part will be described in Section 5 for the interpolation problem over a triangle. Before commencing this derivation, however, we must introduce definitions and notation for the coordinate systems we will use over a triangle. This is the subject of Section 4.

#### 4. Coordinate systems over plane triangles

Let  $T$  be a plane triangle having vertices  $V_1$ ,  $V_2$ , and  $V_3$ . For convenience, we will think of these vertices as being labeled in counterclockwise order. Final results are not sensitive to this assumed ordering.

The indices in the formulas to follow take the values 1, 2, and 3. Index arithmetic is to be interpreted as being cyclic over these three values. For example, if  $i = 3$ , then  $i + 1 = 1$  and  $i + 2 = 2$ .

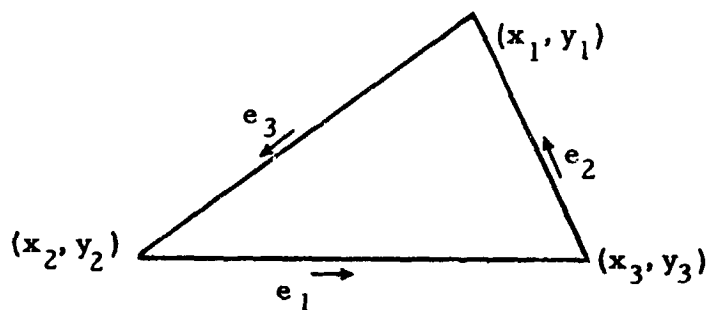
Let  $S_i$  denote the side of the triangle opposite to vertex  $V_i$ . Let  $\theta_i$  denote the interior angle at vertex  $V_i$ , measured from side  $S_{i+2}$  to  $S_{i+1}$ .



In a Euclidean  $(x, y)$ -plane let  $(x_i, y_i)$  be the coordinates of vertex  $V_i$ ,  $i = 1, 2, 3$ .

Introduce directed edge vectors  $e_i$  with components  $u_i$  and  $v_i$  defined by

$$(13) \quad e_i = \overrightarrow{V_{i+1}V_{i+2}} = \begin{bmatrix} u_i \\ v_i \end{bmatrix} = \begin{bmatrix} x_{i+2} - x_{i+1} \\ y_{i+2} - y_{i+1} \end{bmatrix}$$



Denote the Euclidean length of side  $S_i$  by

$$l_i = \|e_i\| = (u_i^2 + v_i^2)^{1/2} \quad i = 1, 2, 3$$

Let  $c_i$  denote the inner product (dot product) of the two edge vectors directed away from vertex  $V_i$ , i. e. the inner product of  $e_{i-1}$  and  $-e_{i+1}$ .

$$\begin{aligned} (14) \quad c_i &= \text{Dot}(\overline{V_i V_{i+1}}, \overline{V_i V_{i-1}}) = \text{Dot}(e_{i-1}, -e_{i+1}) \\ &= -(u_{i-1}u_{i+1} + v_{i-1}v_{i+1}) \\ &= l_{i-1}l_{i+1} \cos \theta_i \quad i = 1, 2, 3 \end{aligned}$$

We note in passing that the  $c_i$ 's and  $l_i$ 's are related by the equations

$$(15) \quad l_i^2 = c_{i-1} + c_{i+1} \quad i = 1, 2, 3$$

$$(16) \quad l_{i+1}^2 - l_{i-1}^2 = c_{i-1} - c_{i+1} \quad i = 1, 2, 3$$

and

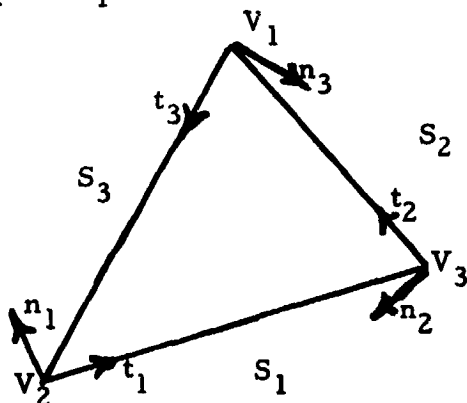
$$(17) \quad 2 c_i = l_{i+1}^2 + l_{i-1}^2 - l_i^2 \quad i = 1, 2, 3$$

Let  $\delta$  denote twice the (signed) area of  $T$ . This quantity is representable as the scalar cross product of any two edge vectors directed away from a common vertex.

$$\begin{aligned}
(18) \quad \delta &= \text{Cross} (\overline{V_i V_{i+1}}, \overline{V_i V_{i-1}}) = \text{Cross} (e_{i-1}, -e_{i+1}) \\
&= \text{Cross} (e_{i+1}, e_{i-1}) \\
&= \det \begin{bmatrix} u_{i+1} & u_{i-1} \\ v_{i+1} & v_{i-1} \end{bmatrix} = u_{i+1} v_{i-1} - v_{i+1} u_{i-1} \\
&= l_{i-1} l_{i+1} \sin \theta_i \quad i = 1, 2, 3
\end{aligned}$$

### Tangential and Normal Coordinates

Relative to side  $S_i$  of the triangle, we introduce an orthogonal coordinate system using coordinates  $(t_i, n_i)$  where  $t_i$  is measured along side  $S_i$  from  $V_{i+1}$  and  $n_i$  is measured positive in the inward normal direction.



The variables  $(t_i, n_i)$  are related to the variables  $(x, y)$  by the equations

$$(19) \quad \begin{bmatrix} t_i \\ n_i \end{bmatrix} = \frac{1}{L_i} \begin{bmatrix} u_i & v_i \\ -v_i & u_i \end{bmatrix} \cdot \begin{bmatrix} x - x_{i+1} \\ y - y_{i+1} \end{bmatrix} \quad i = 1, 2, 3$$

and by the inverse equations



$$(20) \quad \begin{bmatrix} x-x_{i+1} \\ y-y_{i+1} \end{bmatrix} = \frac{1}{l_i} \begin{bmatrix} u_i & -v_i \\ v_i & u_i \end{bmatrix} \cdot \begin{bmatrix} t_i \\ n_i \end{bmatrix} \quad i = 1, 2, 3$$

From Eq. (20) we obtain the partial derivatives

$$(21) \quad \left. \begin{aligned} \partial x / \partial t_i &= u_i / l_i \\ \partial x / \partial n_i &= -v_i / l_i \\ \partial y / \partial t_i &= v_i / l_i \\ \partial y / \partial n_i &= u_i / l_i \end{aligned} \right\} \quad i = 1, 2, 3$$

### Barycentric or Areal Coordinates

Let P be a point with coordinates (x, y). Define the three barycentric (or areal) coordinates of P by:

$$(22) \quad \begin{aligned} r_j &= \text{Cross} (\overline{V_{j+1}V_{j+2}}, \overline{V_{j+1}P}) / \delta \\ &= \text{Cross} (e_j, \overline{V_{j+1}P}) / \delta \\ &= \delta^{-1} \det \begin{bmatrix} u_j & x-x_{j+1} \\ v_j & y-y_{j+1} \end{bmatrix} \\ &= \delta^{-1} [u_j(y-y_{j+1}) - v_j(x-x_{j+1})] \end{aligned} \quad j = 1, 2, 3$$

Note that the quantity computed by the cross product in the formula for  $r_j$  is twice the area of the triangle formed by side j and the point P. Thus the sum of the three cross products used to compute  $r_1$ ,  $r_2$ , and  $r_3$  must be twice the area of T. Therefore, with the normalization factor  $\delta^{-1}$  appearing in the formulas it follows that

$$(23) \quad r_1 + r_2 + r_3 = 1$$

The barycentric coordinates are the unique set of numbers having unit sum and representing P as a linear combination of  $V_1$ ,  $V_2$ , and  $V_3$ , thus

$$\begin{bmatrix} x \\ y \end{bmatrix} = \sum_{j=1}^3 r_j \begin{bmatrix} x_j \\ y_j \end{bmatrix}$$

Each barycentric coordinate  $r_j$  is the unique linear function of  $(x, y)$  that is zero along the line determined by side  $S_j$  and takes the value 1 at the vertex  $V_j$ .

For points inside the triangle T we have all  $r_j \geq 0$  while for points outside there will be some  $r_j < 0$ . The barycentric coordinates of the vertices are:

$$V_1 \sim (1, 0, 0)$$

$$V_2 \sim (0, 1, 0)$$

$$V_3 \sim (0, 0, 1)$$

Using Eq. (22) we may compute partial derivatives as follows:

$$(24) \quad \begin{aligned} \partial r_j / \partial x &= -v_j / \delta \\ \partial r_j / \partial y &= u_j / \delta \end{aligned} \quad j = 1, 2, 3$$

Using Eq. (21) and (24) we obtain further partial derivatives:

$$(25) \quad \begin{aligned} \partial r_j / \partial t_i &= (\partial r_j / \partial x)(\partial x / \partial t_i) + (\partial r_j / \partial y)(\partial y / \partial t_i) \\ &= (-v_j u_i + u_j v_i) / (\delta_i \delta) \\ &= \text{Cross}(e_j, e_i) / (\delta_i \delta) \end{aligned}$$

$$= \begin{cases} 0 & \text{if } j = i \\ 1/\ell_i & \text{if } i-j = 1 \\ -1/\ell_i & \text{if } j-i = 1 \end{cases}$$

$$(26) \quad \partial r_j / \partial n_i = (\partial r_j / \partial x)(\partial x / \partial n_i) + (\partial r_j / \partial y)(\partial y / \partial n_i)$$

$$= (v_j v_i + u_j u_i) / (\ell_i \delta)$$

$$= \text{Dot}(e_j, e_i) / (\ell_i \delta)$$

$$= \begin{cases} \ell_i^2 / (\ell_i \delta) & \text{if } i = j \\ -c_{i-1} / (\ell_i \delta) & \text{if } j-i = 1 \\ -c_{i+1} / (\ell_i \delta) & \text{if } i-j = 1 \end{cases}$$

For more convenient reference, we organize the results of Eq. (25) and (26) into tables as follows:

Table 1 . Values of  $\partial r_j / \partial t_i$

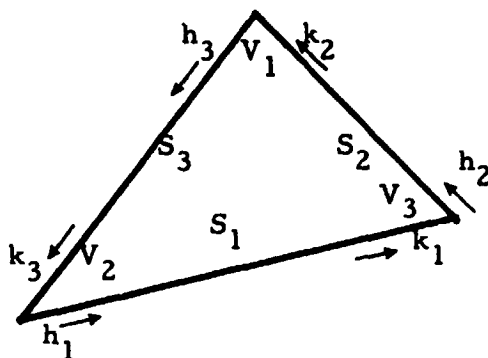
	$/\partial t_1$	$/\partial t_2$	$/\partial t_3$
$\partial r_1 /$	0	$1/\ell_2$	$-1/\ell_3$
$\partial r_2 /$	$-1/\ell_1$	0	$1/\ell_3$
$\partial r_3 /$	$1/\ell_1$	$-1/\ell_2$	0

Table 2 . Values of  $\partial r_j / \partial n_i$

	$/\partial n_1$	$/\partial n_2$	$/\partial n_3$
$\partial r_1 /$	$\ell_1^2 / (\ell_1 \delta)$	$-c_3 / (\ell_2 \delta)$	$-c_2 / (\ell_3 \delta)$
$\partial r_2 /$	$-c_3 / (\ell_1 \delta)$	$\ell_2^2 / (\ell_2 \delta)$	$-c_1 / (\ell_3 \delta)$
$\partial r_3 /$	$-c_2 / (\ell_1 \delta)$	$-c_1 / (\ell_2 \delta)$	$\ell_3^2 / (\ell_3 \delta)$

## 5. Constructing a solution

First convert the given partial derivative data at each vertex to partial derivatives in the directions of the edges meeting at the vertex. For  $i = 1, 2$ , and  $3$ , let  $h_i$  and  $k_i$  respectively denote the values of the first partial derivative with respect to  $t_i$  (the tangential direction along side  $S_i$ ) at  $t_i = 0$  and  $t_i = 1$  (i.e., at the vertices  $V_{i+1}$  and  $V_{i-1}$ ).



The values of  $h_i$  and  $k_i$  are given by

$$(27) \quad \left. \begin{aligned} h_i &= (u_i f_{x, i+1} + v_i f_{y, i+1}) / l_i \\ k_i &= (u_i f_{x, i-1} + v_i f_{y, i-1}) / l_i \end{aligned} \right\} i = 1, 2, 3$$

Henceforth, we may regard  $f_i$ ,  $h_i$ , and  $k_i$  for  $i = 1, 2, 3$ , as defining the data to be interpolated. We proceed by analogy with the discussion of the one-dimensional problem in Section 3. A linear function interpolating the function values  $f_i$ ,  $i = 1, 2, 3$ , is given by

$$w^{(1)} = r_1 f_1 + r_2 f_2 + r_3 f_3$$

Along side  $S_i$ , this function has slope

$$(28) \quad m_i = (f_{i-1} - f_{i+1}) / l_i$$

with respect to the tangential variable  $t_i$ . Subtracting the vertex values and partial derivatives of  $w^{(1)}$  from the given data, we are left with the residual problem of interpolating vertex values of zero and tangential partial derivative values of  $h_i - m_i$  and  $k_i - m_i$ ,  $i = 1, 2, 3$ .

Let us temporarily restrict attention to one side, say side  $S_1$ . On side  $S_1$  we have  $r_1 = 0$ ,  $r_2 = 1 - r_3$ , and  $t_1 = \ell_1 r_3$ . Note that the quadratic function  $r_2 r_3$  reduces to  $r_3(1 - r_3)$ , and the cubic function  $r_2 r_3(r_2 - r_3)$  reduces to  $2r_3(r_3 - \frac{1}{2})(r_3 - 1)$  along side  $S_1$ . [Compare with  $\psi_2$  and  $\psi_3$  of Section 3.] It is easily verified that the partial derivative with respect to  $t_1$  of the scaled function  $\ell_1 r_2 r_3$  has the values 1 and -1 at the vertices  $V_2$  and  $V_3$  respectively. Similarly  $\partial[\ell_1 r_2 r_3(r_2 - r_3)]/\partial t_1$  has the value 1 at  $V_2$  and  $V_3$ .

Thus the function

$$(29) \quad w_1^{(2)} = \frac{h_1 - k_1}{2} \ell_1 r_2 r_3 + \frac{h_1 + k_1 - 2m_1}{2} \ell_1 r_2 r_3(r_2 - r_3)$$

satisfies the residual interpolation requirements on side  $S_1$ ; i.e.,  $w_1^{(2)}$  has zero values at  $V_2$  and  $V_3$  and its partial derivative with respect to  $t_1$  has the values  $h_1 - m_1$ , and  $k_1 - m_1$  at  $V_2$  and  $V_3$  respectively.

On side  $S_2$  we have  $r_2 = 0$ , and thus  $w_1^{(2)}$  and its tangential partial derivative are zero there. Similarly, since  $r_3 = 0$  on side  $S_3$ ,  $w_1^{(2)}$  and its tangential partial derivative are also zero on side  $S_3$ .

By appropriate cycling of indices, define functions  $w_2^{(2)}$  and  $w_3^{(2)}$  analogous to  $w_1^{(2)}$ :

$$(30) \quad w_i^{(2)} = \frac{h_i - k_i}{2} \ell_i r_{i+1} r_{i-1} + \frac{h_i + k_i - 2m_i}{2} \ell_i r_{i+1} r_{i-1} (r_{i+1} - r_{i-1})$$

for  $i = 1, 2, 3$

It follows that the function

$$(31) \quad \bar{w} = w^{(1)} + \sum_{i=1}^3 w_i^{(2)}$$

interpolates the nine items of data  $f_i, h_i, k_i, i=1, 2, 3$ .

Note further that  $\bar{w}$  is exact for quadratic functions since if the data  $f_i, h_i, k_i, i=1, 2, 3$ , arise from a quadratic function it will follow that

$$h_i - m_i = -(k_i - m_i) \quad i = 1, 2, 3$$

so the coefficients of the cubic terms in  $\bar{w}$  vanish leaving  $\bar{w}$  as the unique quadratic function matching the given data.

The function  $\bar{w}$  has a defect however. We require that the partial derivative normal to any side must be a linear function along that side. The cubic functions  $r_{i+1} r_{i-1} (r_{i+1} - r_{i-1}), i=1, 2, 3$ , do not have this property and thus, in general,  $\bar{w}$  does not.

The remedy, described in Goël [1968], is to introduce correction functions  $\rho_i, i=1, 2, 3$ . The function  $\rho_i$  is required to be zero on all three sides of the triangle. It follows that its first partial derivatives in all directions at each vertex are zero. It is further required that the normal derivatives of  $\rho_i$  relative to sides  $S_{i+1}$  and  $S_{i-1}$  be zero on those sides respectively, while the normal derivative of  $\rho_i$  relative to side  $S_i$  is to be a quadratic function along that side. Specifically we can require that

$$(32) \quad \left. \frac{\partial \rho_i}{\partial n_i} \right|_{\text{on side } S_i} = r_{i-1} (1 - r_{i-1}) \ell_i / \delta$$

By adding appropriate multiples of  $\rho_1, \rho_2$ , and  $\rho_3$  to a cubic function, such as  $r_2 r_3 (r_2 - r_3)$ , one can construct a function whose normal partial derivatives on each side are linear functions along the respective sides.

This point will be further developed in the next three sections. In Section 6 we determine the multiples of  $\rho_1$ ,  $\rho_2$ , and  $\rho_3$  needed to correct the function  $r_2 r_3 (r_2 - r_3)$ . In Sections 7 and 8, we discuss two distinct sets of functions having the properties required of the  $\rho_i$ 's.

6. Correcting the normal derivatives of  $g_1 = r_2 r_3 (r_2 - r_3)$

Define

$$g_1 = r_2 r_3 (r_2 - r_3)$$

The partial derivatives of  $g_1$  with respect to the  $r_i$ 's are

$$\partial g_1 / \partial r_1 = 0$$

$$\partial g_1 / \partial r_2 = 2r_2 r_3 - r_3^2$$

$$\partial g_1 / \partial r_3 = r_2^2 - 2r_2 r_3$$

Using the expressions for  $\partial r_i / \partial n_j$  given in Table 2, and evaluating on the indicated sides we obtain:

$$(33) \quad \left. \partial g_1 / \partial n_1 \right|_{\text{on side } S_1} = [3(c_3 - c_2)r_3^2 + 2(2c_2 - c_3)r_3 - c_2] / (\ell_1 \delta)$$

$$(34) \quad \left. \partial g_1 / \partial n_2 \right|_{\text{on side } S_2} = -\ell_2 (1 - r_1)^2 / \delta$$

$$(35) \quad \left. \partial g_1 / \partial n_3 \right|_{\text{on side } S_3} = \ell_3 r_2^2 / \delta$$

We assume the availability of  $C^1$  functions  $\rho_i$ ,  $i=1, 2, 3$ , which have zero values along all edges and satisfy

$$(36) \quad \left. \partial \rho_i / \partial n_j \right|_{\text{on side } S_i} = \begin{cases} r_{i-1}(1-r_{i-1})\ell_i / \delta & \text{if } j=i \\ 0 & \text{if } j=i-1 \text{ or } j=i+1 \end{cases}$$

We wish to determine coefficient  $\alpha_{11}$ ,  $\alpha_{12}$ , and  $\alpha_{13}$  such that the function

$$\tilde{g}_1 = g_1 + \alpha_{11}\rho_1 + \alpha_{12}\rho_2 + \alpha_{13}\rho_3$$



will have the property that for  $j = 1, 2, 3$ , the normal derivative  $\partial \tilde{g}_1 / \partial n_j$  is a linear function along side  $S_j$ . Comparing the quadratic terms in Eqs. (33), (34), and (35) with the quadratic term in Eq. (36) it follows that the appropriate values for the  $\alpha_{1j}$ 's are

$$\alpha_{11} = 3(c_3 - c_2) / l_1^2 = 3(l_2^2 - l_3^2) / l_1^2$$

$$\alpha_{12} = -1$$

and

$$\alpha_{13} = 1$$

Using these values of the  $\alpha_{1j}$ 's one can obtain the following equations showing the linear character of the normal derivatives of  $l_1 \tilde{g}_1$  on the respective sides:

$$\left. \partial(l_1 \tilde{g}_1) / \partial n_1 \right|_{\text{on side } S_1} = [(c_3 + c_2)r_3 - c_2] / \delta$$

$$= (c_3 r_3 - c_2 r_2) / \delta$$

$$= \frac{r_3}{\tan \theta_3} - \frac{r_2}{\tan \theta_2}$$

$$\left. \partial(l_1 \tilde{g}_1) / \partial n_2 \right|_{\text{on side } S_2} = -l_1 l_2 (1 - r_1) / \delta = -l_1 l_2 r_3 / \delta$$

$$= -r_3 / \sin \theta_3$$

$$\left. \partial(l_1 \tilde{g}_1) / \partial n_3 \right|_{\text{on side } S_3} = l_1 l_3 r_2 / \delta = r_2 / \sin \theta_2$$

Collecting the results of this section and cycling the indices appropriately we define

$$(37) \quad \tilde{g}_i = r_{i+1}r_{i-1}(r_{i+1}-r_{i-1}) + \frac{3(l_{i+1}^2 - l_{i-1}^2)}{l_i^2} \rho_i - \rho_{i+1} + \rho_{i-1}$$

$$i = 1, 2, 3$$

Each function  $\tilde{g}_i$  has the same interpolatory properties as the simpler cubic function  $r_{i+1}r_{i-1}(r_{i+1}-r_{i-1})$  at the three vertices and has the additional property that  $\partial \tilde{g}_i / \partial n_j$  is a linear function along side  $S_j$  for all  $i$  and  $j$ .

Therefore for our complete interpolation formula we replace Eq (31) by

$$(38) \quad w = \sum_{i=1}^3 \left[ r_i f_i + \frac{h_i - k_i}{2} l_i r_{i-1} r_{i+1} + \frac{h_i + k_i - 2m_i}{2} l_i \tilde{g}_i \right]$$

7. A set of rational correction functions,  $\rho_i$

Define

$$(39) \quad \rho_i = r_i r_{i+1}^2 r_{i-1}^2 / [(1-r_{i+1})(1-r_{i-1})] \quad i = 1, 2, 3$$

This set of rational functions is discussed by Goël [1968] who attributes their use in this context to Zienkiewicz [1957].

For convenience consider the single function

$$\rho_1 = r_1 r_2^2 r_3^2 / [(1-r_2)(1-r_3)]$$

Over the triangle, T, the denominator of  $\rho_1$  vanishes only at the vertex  $V_2$ , where  $r_2 = 1$ , and at  $V_3$ , where  $r_3 = 1$ . These are removable singularities however since, for example, at  $V_2$  the numerator has a third order zero ( $r_1 = 0$  and  $r_3 = 0$ ) and thus  $\rho_1$  has a second order zero at  $V_2$ . Similarly  $\rho_1$  vanishes to second order at  $V_3$ .

At all other edge points it is clear that  $\rho_1$  vanishes because it contains  $r_1$ ,  $r_2$ , and  $r_3$  as factors.

To verify that the normal partial derivatives of  $\rho_i$  have the necessary properties compute

$$\partial \rho_1 / \partial r_1 = \rho_1 / r_1$$

$$\partial \rho_1 / \partial r_2 = (2-r_2) \rho_1 / [r_2(1-r_2)]$$

$$\partial \rho_1 / \partial r_3 = (2-r_3) \rho_1 / [r_3(1-r_3)]$$

Then using expressions for  $\partial r_i / \partial n_j$  from Table 2, one finds

$$\left. \frac{\partial \rho_1}{\partial n_1} \right|_{\text{on side } S_1} = r_3(1-r_3)\ell_1/\delta$$

$$\left. \frac{\partial \rho_1}{\partial n_2} \right|_{\text{on side } S_2} = 0$$

$$\left. \frac{\partial \rho_1}{\partial n_3} \right|_{\text{on side } S_3} = 0$$

It is thus verified that the rational functions of Eq(39) can be used as the correction functions  $\rho_i$  described in Section 5.

To compute values of  $\rho_i$ ,  $i = 1, 2, 3$ , assume values of  $r_i$ ,  $i = 1, 2, 3$ , and

$$(40) \quad \varphi_i = r_{i+1}r_{i-1} \quad i = 1, 2, 3$$

are given. One then computes

$$\psi := r_1\varphi_1$$

$$\hat{r}_i := 1-r_i \quad i = 1, 2, 3$$

{If any  $\hat{r}_i = 0$  branch to handle the special trivial case of interpolation at a vertex}

$$\rho_i := \psi\varphi_i/(\hat{r}_{i+1}\hat{r}_{i-1}) \quad i = 1, 2, 3$$

Thus the computation of the rational  $\rho_i$ 's requires 7 multiplications, 3 additions, 3 divisions, and 3 zero tests.

8. A set of piecewise cubic correction functions,  $\rho_i$

Define

$$(41) \quad \rho_i = \begin{cases} r_i[6r_{i+1}r_{i-1} + r_i(5r_i - 3)]/6 & \text{if } r_i = \min\{r_1, r_2, r_3\} \\ r_{i+1}^2(-r_{i+1} + 3r_{i-1})/6 & \text{if } r_{i+1} = \min\{r_1, r_2, r_3\} \\ r_{i-1}^2(-r_{i-1} + 3r_{i+1})/6 & \text{if } r_{i-1} = \min\{r_1, r_2, r_3\} \end{cases}$$

for  $i = 1, 2, 3$

Each function  $\rho_i$  consists of a set of three cubic functions which match with  $C^1$  continuity along internal boundary lines connecting the vertices to the centroid of the triangle  $T$ . This set of functions is discussed by Goël [1968] who attributes their use in this context to Clough and Tocher [1965].

Along side  $S_1$  we have  $r_1 = \min\{r_1, r_2, r_3\}$  and thus

$$\rho_1 = r_1[6r_2r_3 + r_1(5r_1 - 3)]/6$$

In this region the derivatives  $\partial\rho_1/\partial r_i$  are given by

$$\partial\rho_1/\partial r_1 = [6r_2r_3 + 15r_1^2 - 6r_1]/6$$

$$\partial\rho_1/\partial r_2 = r_1r_3$$

$$\partial\rho_1/\partial r_3 = r_1r_2$$

Using the expressions for  $\partial r_i/\partial n_1$  from Table 2, we find

$$\left. \frac{\partial\rho_1}{\partial n_1} \right|_{\text{on side } S_1} = r_3(1-r_3)l_1/6$$

It can also be verified that

$$\left. \frac{\partial \rho_1}{\partial n_2} \right|_{\text{on side } S_2} = 0$$

and

$$\left. \frac{\partial \rho_1}{\partial n_3} \right|_{\text{on side } S_3} = 0$$

Thus the piecewise cubic functions of Eq (41) have the properties need for use as the correction functions  $\rho_i$  of Section 5.

If Eq (41) is used in a computer program the usual situation will be that for one set of values of  $r_1$ ,  $r_2$ , and  $r_3$  the program must compute values of  $\rho_1$ ,  $\rho_2$ , and  $\rho_3$ . In this context the following restatement of Eq(41) is useful:

Let  $m$  be an index such that  $r_m = \min\{r_1, r_2, r_3\}$ . Then

$$\rho_m = r_m[6r_{m+1}r_{m-1} + r_m(5r_m - 3)]/6$$

$$\rho_{m+1} = r_m^2(-r_m + 3r_{m-1})/6$$

$$\rho_{m-1} = r_m^2(-r_m + 3r_{m+1})/6$$

To compute values of  $\rho_i$ ,  $i=1, 2, 3$ , given  $r_i$ ,  $i=1, 2, 3$ , and

$$\varphi_i = r_{i+1}r_{i-1} \quad i = 1, 2, 3$$

the following steps can be used:

Find  $m$  such that  $r_m = \min\{r_1, r_2, r_3\}$

$$a := \frac{1}{2} r_m^2$$

$$b := \frac{1}{3} r_m$$

$$\rho_m := r_m(\varphi_m + \frac{5}{3} a) - a$$

$$\rho_{m+1} := a(r_{m-1} - b)$$

$$\rho_{m-1} := a(r_{m+1} - b)$$

Two compares are required to determine  $m$ . Counting these as additions, the computation of the piecewise cubic correction functions,  $\rho_i$ , requires seven multiplications and six additions.

## 9. Transforming formulas to algorithms

Assume that data  $(x_i, y_i, f_i, f_{x,i}, f_{y,i})$ ,  $i = 1, 2, 3$  is given, where  $(x_i, y_i)$  specifies the coordinates of the vertex  $V_i$  and  $(f_i, f_{x,i}, f_{y,i})$  specifies the value of the function and its first partial derivatives with respect to  $x$  and  $y$  at the vertex  $V_i$ . The vertices  $V_i$  should not be colinear. Either counterclockwise or clockwise ordering of the vertices is acceptable.

Further assume a coordinate pair,  $(x, y)$ , is given at which an interpolated value,  $w$ , is to be computed. The point  $(x, y)$  should not be exterior to the triangle  $T$  having vertices  $V_1, V_2$ , and  $V_3$ .

We will describe the interpolation algorithm in three phases. Phase 1 will compute the preliminary quantities,  $u_i, v_i, l_i^2, \delta^{-1}, r_i$ , and  $\phi_i$ ,  $i = 1, 2, 3$ . Phase 2 will be the computation of the  $\rho_i$ 's using either the method of Section 7 or of Section 8. Phase 3 will complete the interpolation. We will describe three versions of Phase 3.

All index expressions such as  $i+1$  and  $i-1$  must be interpreted cyclicly so that the resulting index value is 1, 2, or 3. The name "det" is used to indicate computation of the determinant of a matrix. Phase 1 of the algorithm proceeds as follows:

Begin Phase 1

$$\left. \begin{aligned} u_i &:= x_{i-1} - x_{i+1} \\ v_i &:= y_{i-1} - y_{i+1} \\ l_i^2 &:= u_i^2 + v_i^2 \end{aligned} \right\} \quad i = 1, 2, 3$$

$$\delta := \det \begin{bmatrix} u_1 & u_2 \\ v_1 & v_2 \end{bmatrix}$$

{Test for the error condition,  $\delta=0$ , indicating colinearity of the of the vertices. }



$$\tilde{x} := x - x_1$$

$$\tilde{y} := y - y_1$$

$$r_2 := \delta^{-1} \det \begin{bmatrix} u_2 & \tilde{x} \\ v_2 & \tilde{y} \end{bmatrix}$$

$$r_3 := \delta^{-1} \det \begin{bmatrix} u_3 & \tilde{x} \\ v_3 & \tilde{y} \end{bmatrix}$$

$$r_1 := 1 - (r_2 + r_3)$$

{If one wishes to test for the possibility that  $(x, y)$  is exterior to the triangle the test can be made here. The condition  $r_i < 0$  for any  $i$  indicates that  $(x, y)$  is exterior to the triangle. }

$$\varphi_i := r_{i+1} r_{i-1} \quad i = 1, 2, 3$$

End Phase 1

Note that Phase 1 requires 17 multiplications, 16 additions, and one division.

Phase 2 consists of the computation of the  $\rho_i$ 's using either the method of Section 7 or of Section 8. We proceed to the discussion of Phase 3.

The divisor  $l_i$  in Eq. (27), and (28) will cancel with the multiplier  $l_i$  in Eq (38). Thus instead of computing  $h_i$  and  $k_i$  we will compute quantities  $\tilde{h}_i$  and  $\tilde{k}_i$  such that  $h_i = \tilde{h}_i / l_i$  and  $k_i = \tilde{k}_i / l_i$ .

Version 1 of Phase 3 is the following:

### Phase 3, Version 1

$$\left. \begin{aligned}
 \tilde{h}_i &:= u_i f_{x,i+1} + v_i f_{y,i+1} \\
 \tilde{k}_i &:= u_i f_{x,i-1} + v_i f_{y,i-1} \\
 \tilde{g}_i &:= (r_{i+1} - r_{i-1}) \varphi_i + 3 \frac{l_{i+1}^2 - l_{i-1}^2}{l_i^2} \rho_i - \rho_{i+1} + \rho_{i-1}
 \end{aligned} \right\} \quad i = 1, 2, 3$$

$$w := \sum_{i=1}^3 f_i r_i + \frac{1}{2} (\tilde{h}_i - \tilde{k}_i) \varphi_i + \left[ \frac{1}{2} (\tilde{h}_i + \tilde{k}_i) - f_{i-1} + f_{i+1} \right] \tilde{g}_i$$

Phase 3, Version 1, requires 36 multiplications, 42 additions, and 3 divisions. This includes six multiplications by one half. The computation can be rearranged so that there is only one multiplication by one half. This leads to what we will call Phase 3, Version 2 which requires 31 multiplications, 43 additions, and 3 divisions.

Version 2 differs from Version 1 only in the expression for  $w$  which changes to:

$$w := \sum_{i=1}^3 f_i (r_i + \tilde{g}_{i-1} - \tilde{g}_{i+1}) + \frac{1}{2} \sum_{i=1}^3 \tilde{h}_i (\tilde{g}_i + \varphi_i) + \tilde{k}_i (\tilde{g}_i - \varphi_i)$$

From this point it takes only a little more rearrangement to obtain a formulation which explicitly uses cardinal functions for the given data  $(f_i, f_{x,i}, f_{y,i})$ ,  $i = 1, 2, 3$ . This formulation, which we will call Phase 3, Version 3, uses the same number of multiplications, additions, and divisions as Version 2.

Phase 3, Version 3

$$\begin{aligned}
 \tilde{g}_i &:= (r_{i+1} - r_{i-1})\varphi_i + 3 \frac{l_{i+1}^2 - l_{i-1}^2}{l_i^2} \rho_i - \rho_{i+1} + \rho_{i-1} \\
 p_i &:= \tilde{g}_i + \varphi_i \\
 q_i &:= \tilde{g}_i - \varphi_i
 \end{aligned}
 \left. \vphantom{\begin{aligned} \tilde{g}_i \\ p_i \\ q_i \end{aligned}} \right\} i = 1, 2, 3$$
  

$$\begin{aligned}
 \alpha_i &:= r_i + \tilde{g}_{i-1} - \tilde{g}_{i+1} \\
 \tilde{\beta}_i &:= u_{i-1}p_{i-1} + u_{i+1}q_{i+1} \\
 \tilde{\gamma}_i &:= v_{i-1}p_{i-1} + v_{i+1}q_{i+1}
 \end{aligned}
 \left. \vphantom{\begin{aligned} \alpha_i \\ \tilde{\beta}_i \\ \tilde{\gamma}_i \end{aligned}} \right\} i = 1, 2, 3$$
  

$$w := \sum_{i=1}^3 f_i \alpha_i + \frac{1}{2} \sum_{i=1}^3 (f_{x,i} \tilde{\beta}_i + f_{y,i} \tilde{\gamma}_i)$$

Version 3 is particularly efficient for the case in which there are a number of functions to be interpolated at the same interpolation point,  $(x, y)$ . In such a case only the final formula for  $w$  must be recomputed for each function to be interpolated.

The explicit computation of the cardinal functions,  $\alpha_i$ ,  $\frac{1}{2}\tilde{\beta}_i$ , and  $\frac{1}{2}\tilde{\gamma}_i$ , as provided by Version 3, is needed in applications in which the quantities  $f_i$ ,  $f_{x,i}$ , and  $f_{y,i}$  are unknowns to be solved for. This is the situation in the finite element methods for solving partial differential equations and in the fitting of a smooth surface to noisy data.

10. The method described in Goël [1968]

For comparison with the results of Section 9 we will give a brief description of the interpolation method given in Goël [1968]. This method is attributed by Goël to Clough and Tocher [1965] and Zienkiewicz [1967].

We refer primarily to Eq (28) and (34) of Goël [1968]. The following change of notation will convert Goël's symbols to ours.

Goël's notation	Notation of this paper
$x'$	$r_2$
$y'$	$r_3$
$1-x'-y'$	$r_1$
$\rho_i$	$-\rho_i/6$
$\alpha_i, \beta_i, \gamma_i$	$\hat{\alpha}_i, \hat{\beta}_i, \hat{\gamma}_i$
$\tilde{\alpha}_i, \tilde{\beta}_i, \tilde{\gamma}_i$	$\alpha_i, \beta_i, \gamma_i$
$\Delta$	$\delta/2$
$L_i, C_i$	$l_i, c_i$

We will indicate precomputation of the common subexpressions in Goël's formulas in order to provide a basis for obtaining a realistic operation count. The quantities computed in Phases 1 and 2 [see Section 9] are all needed for Goël's formulas so we will assume these computations have been done and proceed to describe Phase 3.

### Phase 3, Gočl

$$\eta_i := r_i^2 (2r_{i+1} - 3)$$

$$\tilde{\rho}_i := \rho_i / \ell_i^2$$

$$\psi := r_1 \varphi_1$$

$$\left. \begin{aligned} \hat{\alpha}_i &:= 1 + \eta_{i+1} + \eta_{i-1} - 2 [\rho_i - 2 (\rho_{i+1} + \rho_{i-1} - \psi)] \\ \hat{\beta}_i &:= r_i \varphi_{i-1} + \frac{1}{2} [\psi - \rho_i - 5\rho_{i+1} + 3\rho_{i-1}] \\ \hat{\gamma}_i &:= r_i \varphi_{i+1} + \frac{1}{2} [\psi - \rho_i + 3\rho_{i+1} - 5\rho_{i-1}] \end{aligned} \right\} i = 1, 2, 3$$

$$\left. \begin{aligned} \alpha_i &:= \hat{\alpha}_i - (\rho_{i+1} + \rho_{i-1})(u_{i+1}u_{i-1} + v_{i+1}v_{i-1}) \\ \beta_i &:= u_{i-1}\hat{\beta}_i - u_{i+1}\hat{\gamma}_i + \frac{1}{2}\delta(v_{i+1}\tilde{\rho}_{i+1} + v_{i-1}\tilde{\rho}_{i-1}) \\ \gamma_i &:= v_{i-1}\hat{\beta}_i - v_{i+1}\hat{\gamma}_i - \frac{1}{2}\delta(u_{i+1}\tilde{\rho}_{i+1} + u_{i-1}\tilde{\rho}_{i-1}) \end{aligned} \right\} i = 1, 2, 3$$

$$w := \sum_{i=1}^3 (f_i \alpha_i + f_{x,i} \beta_i + f_{y,i} \gamma_i)$$

Assuming the quantities  $\frac{1}{2}\delta$ ,  $3\rho_i$ , and  $5\rho_i$ , would be computed only once each, the operation count for Phase 3, Gočl, is 71 multiplications, 81 additions, and 3 divisions.

It can be verified, by the appropriate tedious algebra, that  $\alpha_i$ ,  $\beta_i$ , and  $\gamma_i$  as defined above are identical with  $\alpha_i$ ,  $\frac{1}{2}\tilde{\beta}_i$ , and  $\frac{1}{2}\tilde{\gamma}_i$  as defined in Phase 3, Version 3 [Section 9]. Thus the interpolated value,  $w$ , is the same by either method.

11. Summary of operation counts

	Multiplications	Additions	Divisions
Phase 1	17	16	1
Phase 2 using rational $\rho_i$ 's	7	3	3
Phase 2 using piecewise cubic $\rho_i$ 's	7	6	0
Phase 3, Version 1	36	42	3
Phase 3, Versions 2 or 3	31	43	3
Phase 3, Goël	71	81	3
Totals using piecewise cubic $\rho_i$ 's :			
Version 1	60	64	4
Versions 2 or 3	55	65	4
Goël	95	103	4

If we weight the multiplications, additions, and divisions in the ratio 2:1:6, then the operation count for Versions 2 or 3 is 63% of the count for Goël's version.

### References

Birkhoff, Garrett, and Mansfield, Lois, 1974, Compatible Triangular Finite Elements, Jour. Math. Anal. and Appl., 47, 531-553.

Clough, R.W., and Tocher, J.L. 1965, Finite Element Stiffness Matrices for Analysis of Plates in Bending, Proc. Conf. Matrix Methods in Struct. Mech., Air Force Inst. of Tech., Wright-Patterson A.F.B., Ohio.

Goël, J. -J., 1968, Construction of Basic Functions for Numerical Utilisation of Ritz's Method, Numerische Mathematik, 12, 435-447.

Lawson, C. L., 1972, Generation of a Triangular Grid with Application to Contour Plotting, Jet Propulsion Laboratory, Section 914 Tech. Memo. No. 299, 24 pp. (an internal report).

Zienkiewicz, O.C., 1967, The Finite Element Method in Structural and Continuum Mechanics, McGraw Hill (A 2nd edition appeared in 1971, however it is the 1967 edition that is referenced by Goël [1968]).